

# Modelling the thermodynamic equilibrium of struvite precipitation as an alternative to remove and recover P from nutrient rich wastewater

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## PROBLEM STATEMENT



P: the limiting resource of agriculture



Eutrophication



Uncontrolled struvite deposition

## INTRODUCTION

Anaerobic treatment of agroindustrial wastes -like slaughterhouse wastewater- is a powerful technology to remove the organic content. However the nutrient content of the treated wastewater or the anaerobically digested dewatering liquid remains almost unchanged. Excess of nutrients may cause eutrophication of aquatic systems, difficulties for water supply and crystalline deposits by uncontrolled deposition of phosphate salts in the treatment systems. Nutrient recovery has become more important in recent years as demand increases. Recovery is particularly important for P, as it is becoming an increasingly limited resource.

## OBJECTIVE

Predict potential nutrient removal from a wastewater stream of known chemical composition and under defined operating precipitation conditions to design the crystallization reactors and to define the optimum operating conditions for each influent and to evaluate the operational efficiency.

## STRUVITE PRECIPITATION



Ionization fraction:

$$\alpha_{ion}^{charge} = \frac{C_{free\_ion}}{C_{T,free+combined}}$$

To precipitate Supersaturation > 1:

$$S_c = \left( \frac{P_s}{P_{seq}} \right)^{1/3} > 1$$

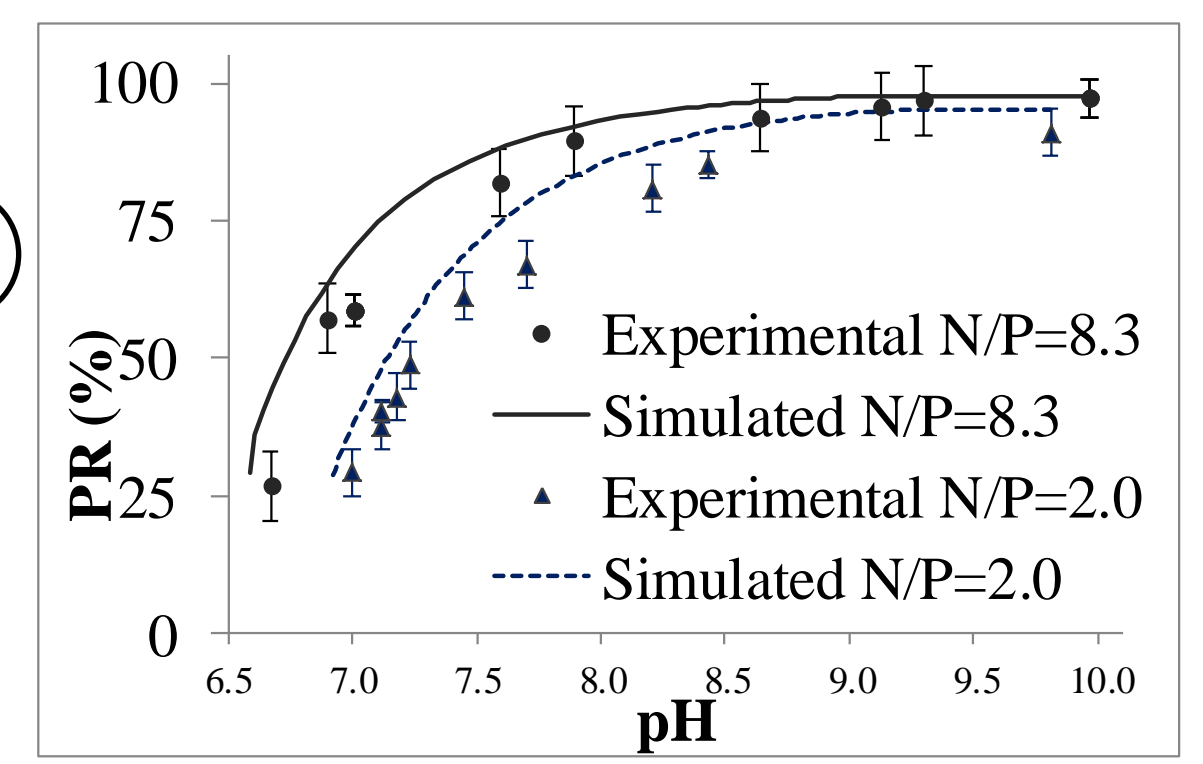
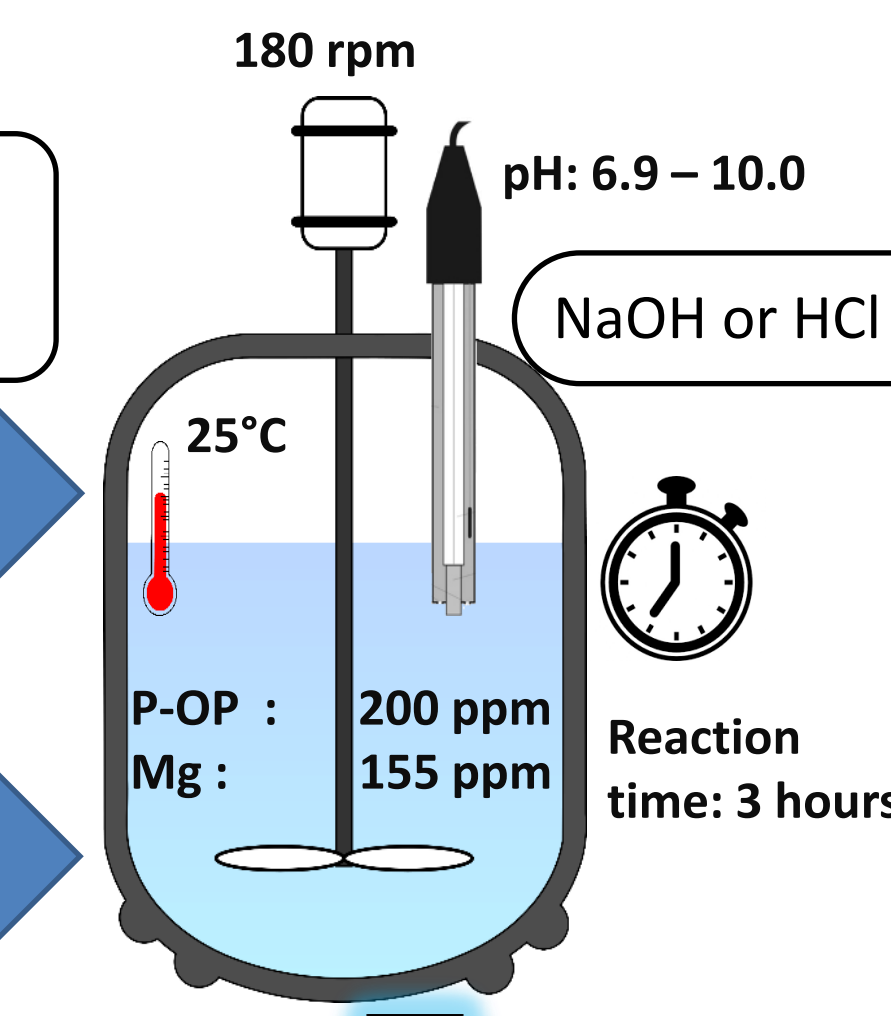
## MODEL VALIDATION

Synthetic wastewater solution:  
(NH<sub>4</sub>)<sub>2</sub>HPO<sub>4</sub>  
NH<sub>4</sub>Cl

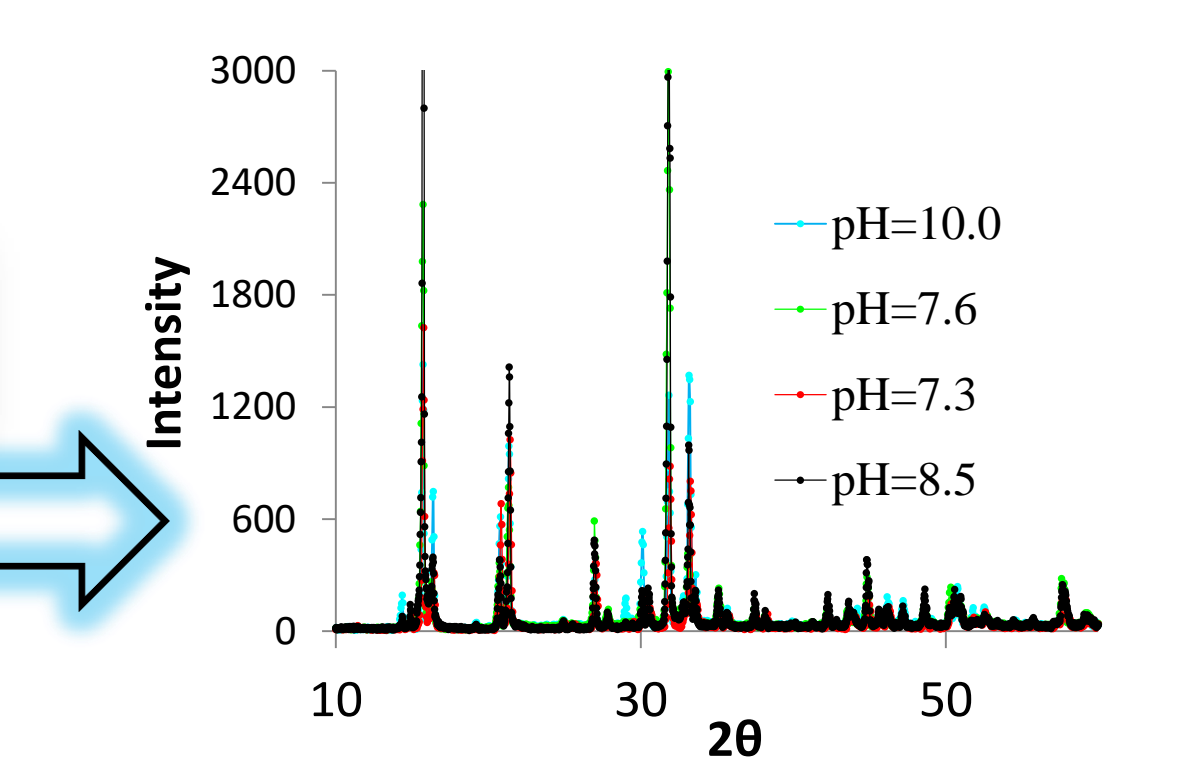
Mg/P = 1.0

N/P = 2.0 and 8.3

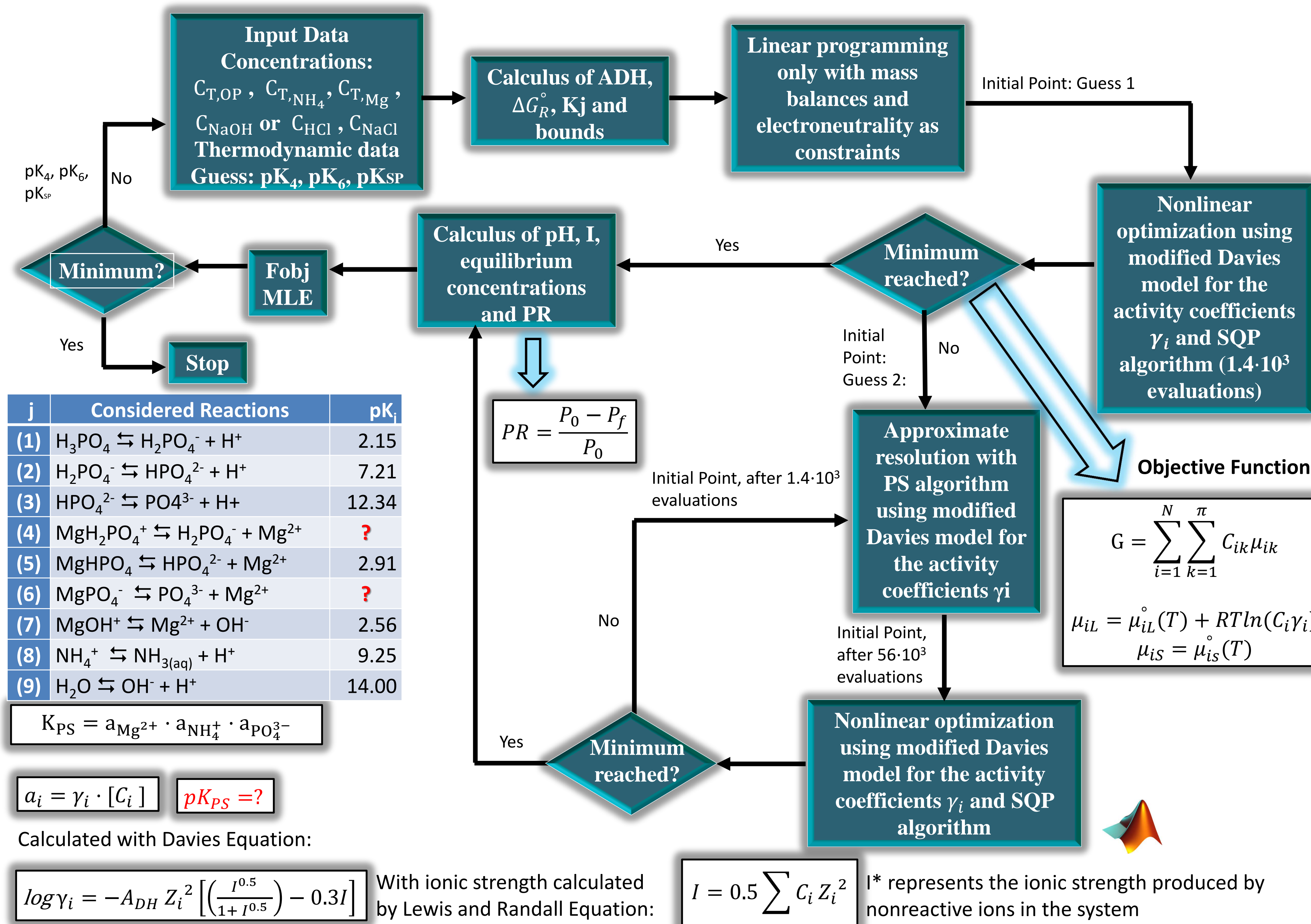
MgCl<sub>2</sub>·6H<sub>2</sub>O



Predicted and measured PR (%) as struvite for P-OP=200 ppm, Mg/P=1 for N/P=2.0 and N/P=8.3 at T=25°C.



## THERMODYNAMIC MODEL FORMULATION



j	Considered Reactions	pK <sub>i</sub>
(1)	H <sub>3</sub> PO <sub>4</sub> ⇌ H <sub>2</sub> PO <sub>4</sub> <sup>-</sup> + H <sup>+</sup>	2.15
(2)	H <sub>2</sub> PO <sub>4</sub> <sup>-</sup> ⇌ HPO <sub>4</sub> <sup>2-</sup> + H <sup>+</sup>	7.21
(3)	HPO <sub>4</sub> <sup>2-</sup> ⇌ PO <sub>4</sub> <sup>3-</sup> + H <sup>+</sup>	12.34
(4)	MgH <sub>2</sub> PO <sub>4</sub> <sup>+</sup> ⇌ H <sub>2</sub> PO <sub>4</sub> <sup>-</sup> + Mg <sup>2+</sup>	?
(5)	MgHPO <sub>4</sub> ⇌ HPO <sub>4</sub> <sup>2-</sup> + Mg <sup>2+</sup>	2.91
(6)	MgPO <sub>4</sub> ⇌ PO <sub>4</sub> <sup>3-</sup> + Mg <sup>2+</sup>	?
(7)	MgOH <sup>+</sup> ⇌ Mg <sup>2+</sup> + OH <sup>-</sup>	2.56
(8)	NH <sub>4</sub> <sup>+</sup> ⇌ NH <sub>3(aq)</sub> + H <sup>+</sup>	9.25
(9)	H <sub>2</sub> O ⇌ OH <sup>-</sup> + H <sup>+</sup>	14.00

$$K_{PS} = a_{Mg^{2+}} \cdot a_{NH_4^+} \cdot a_{PO_4^{3-}}$$

$$a_i = \gamma_i \cdot [C_i] \quad pK_{PS} = ?$$

Calculated with Davies Equation:

$$\log \gamma_i = -A_{DH} Z_i^2 \left[ \left( \frac{I^{0.5}}{1+I^{0.5}} \right) - 0.3I \right]$$

With ionic strength calculated by Lewis and Randall Equation:

$$I = 0.5 \sum C_i Z_i^2 \quad I^* \text{ represents the ionic strength produced by nonreactive ions in the system}$$

## CONCLUSIONS

- A hybrid optimization procedure combining Pattern Search (PS) + Sequential Quadratic Programming (SQP) algorithm has been developed to minimize Gibbs free Energy and to predict the potential P-OP removal as struvite from wastewater.
- The maximum likelihood estimation method (MLE) was applied to estimate the pK for reactions 4, 6 and pK<sub>PS</sub> resulting: 0.45, 6.58 and 13.26 respectively, according to [1], [2] and [3].
- Excess of Mg improve PR although this improvement is least significant as Mg/P increases. The positive impact in PR produced by increase in Mg/P is more significant at lower N/P and higher I\*.
- PR decreases with the N-NH<sub>4</sub><sup>+</sup> concentration. The relative percentage reduction is more pronounced at low pH, low Mg/P and high I\*.
- The increase in I\* produces a decrease in the achieved PR for the same operational conditions. This negative impact is more relevant at low pH, N/P and Mg/P molar ratios.
- For the conditions considered typical of anaerobically digested sludge dewatering liquid (N-NH<sub>4</sub><sup>+</sup> = 750 ppm and P-OP=200 ppm with I\* = 0.15 M) the highest relative improve in PR respect to Mg/P stoichiometric relations is achieved at a molar ratio Mg/P=1.5. The maximum PR obtained was 99.46% at pH=8.56.

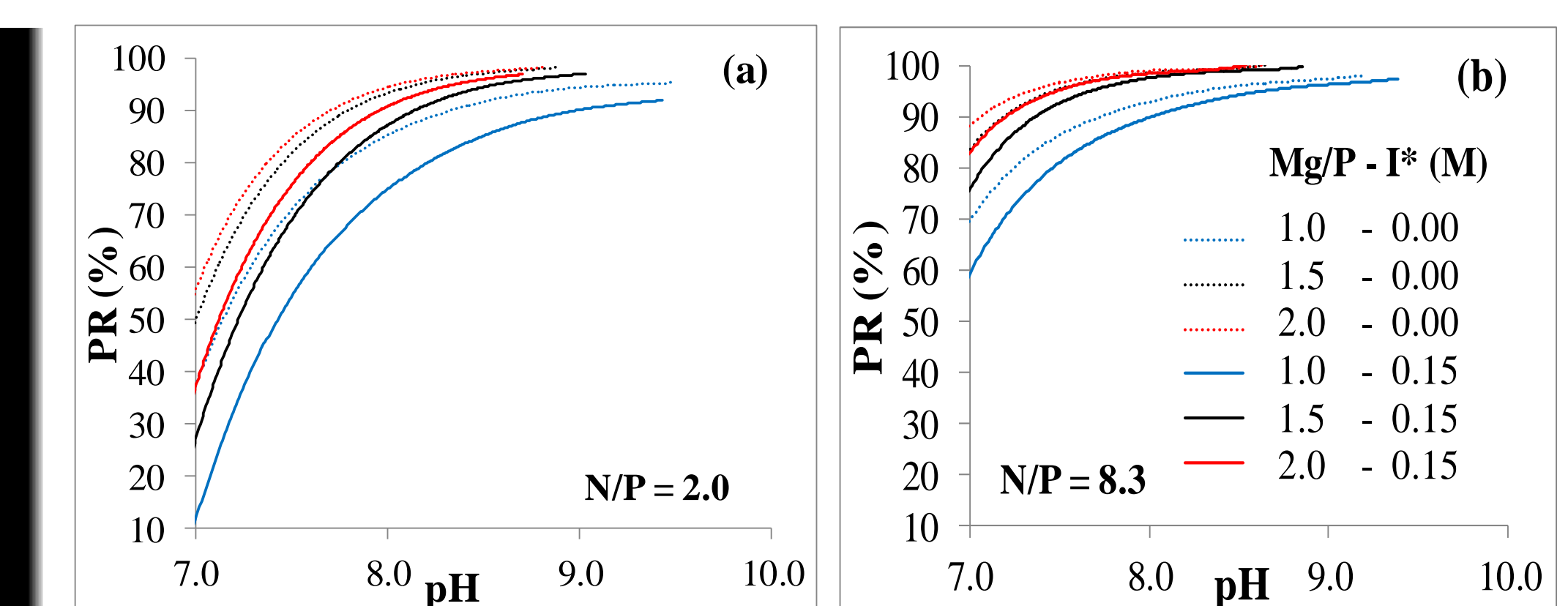
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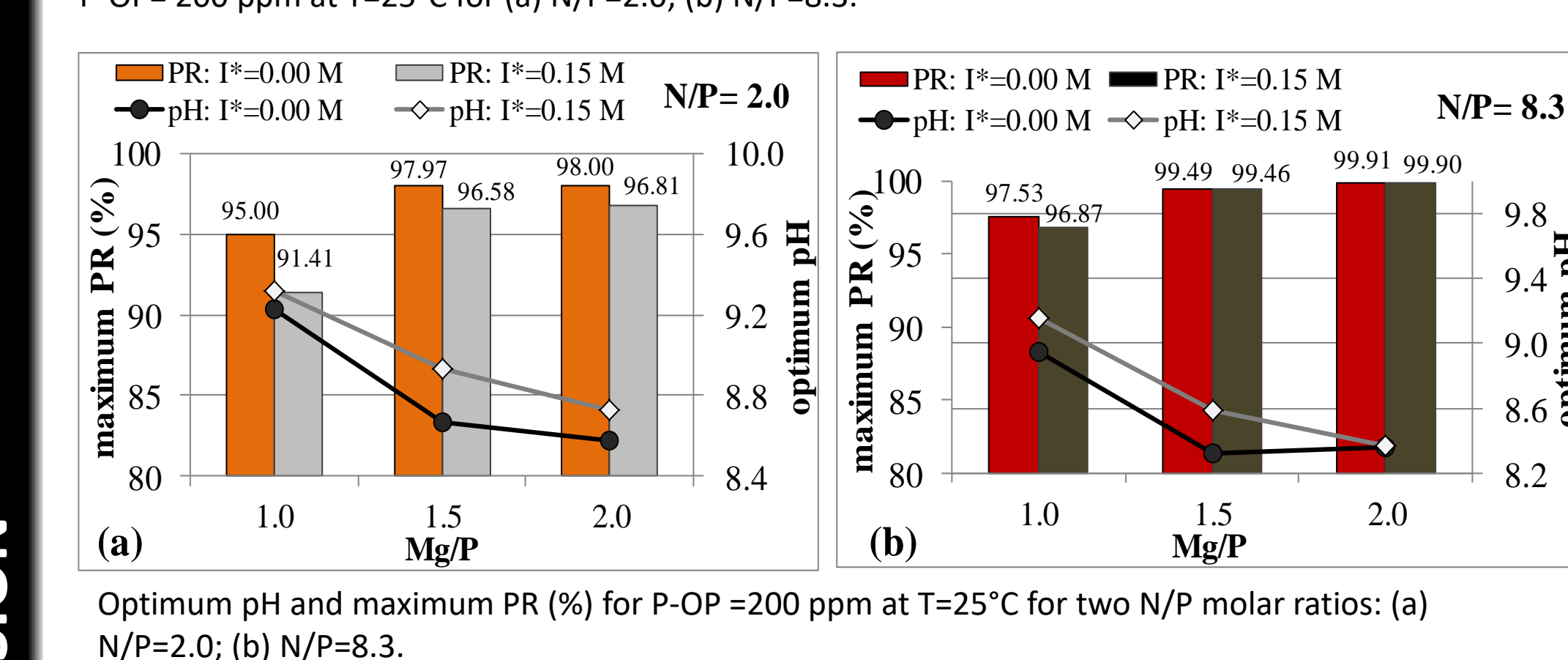
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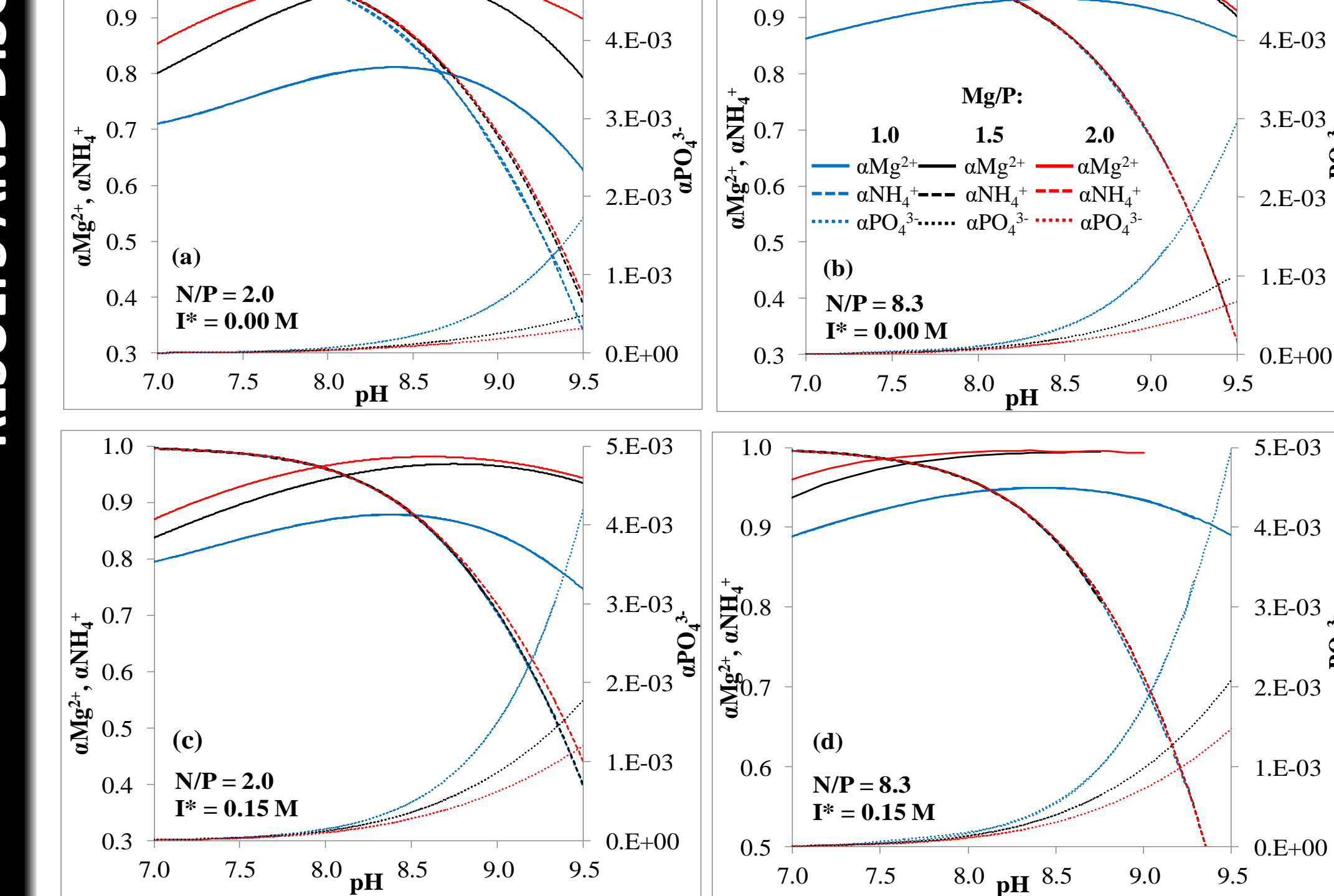
## RESULTS AND DISCUSSION



Influence of molar ratios Mg/P (1.0, 1.5 and 2.0), pH (7.0-10.0) and I\* (0.00 M, 0.15 M) on the PR for P-OP = 200 ppm at T=25°C for (a) N/P=2.0; (b) N/P=8.3.



Optimum pH and maximum PR (%) for P-OP = 200 ppm at T=25°C for two N/P molar ratios: (a) N/P=2.0; (b) N/P=8.3.



Ionization fraction at different equilibrium pH and Mg/P molar ratios for P-OP=200 ppm and T=25°C with (a) N/P=2.0, I\*=0.00 M; (b) N/P=8.3, I\*=0.00 M; (c) N/P=2.0, I\*=0.15 M; (d) N/P=8.3, I\*=0.15 M.

Initially ↑ pH produces ↑ PR likely due to ↑ of free PO<sub>4</sub><sup>3-</sup> as a consequence of the successive deprotonation of HPO<sub>4</sub><sup>2-</sup>, H<sub>2</sub>PO<sub>4</sub><sup>-</sup> and H<sub>3</sub>PO<sub>4</sub>. This ↑ in PR is counteracted by ↓ in the free NH<sub>4</sub><sup>+</sup> which is transformed to NH<sub>3</sub>.  
↑ Mg/P ↑ PR, due to a ↑ of free Mg<sup>2+</sup>. At higher pH, the ↑ in PR is less sensitive to Mg/P, because the negative effect produced by ↓ NH<sub>4</sub><sup>+</sup> prevails.  
↑ I produces ↑ in free Mg<sup>2+</sup>, PO<sub>4</sub><sup>3-</sup> and NH<sub>4</sub><sup>+</sup>. This ↑ is not sufficient to counteract the ↑ in γ of struvite components produced by the high charges Z from these ions.